

PhD Defense

Uncertainty quantification
methodology for seismic fragility
curves of mechanical structures

-
Application to a piping system of a
nuclear power plant

Clément GAUCHY (CEA, CMAP), Cyril
FEAU (CEA), Josselin GARNIER (CMAP)

Seismic probabilistic risk assessment (SPRA) is dedicated to estimating the safety of a mechanical structure subjected to seismic ground motions and consists in three main steps ¹:

- **1)** Estimation of the probability measure λ of annual occurrence of a seismic ground motion of intensity $a \in \mathbb{R}^+$. \leftrightarrow Probabilistic Seismic Hazard Analysis (PSHA);

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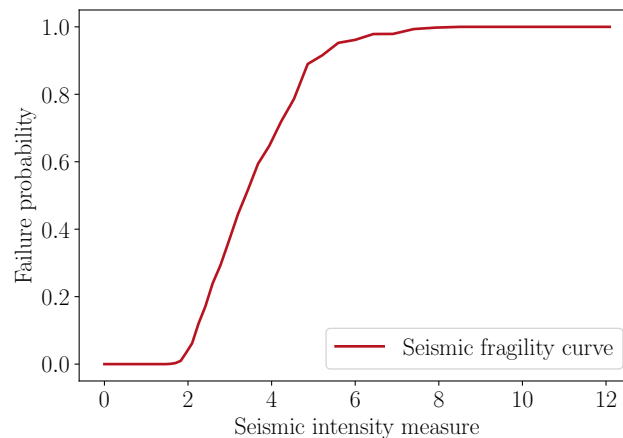
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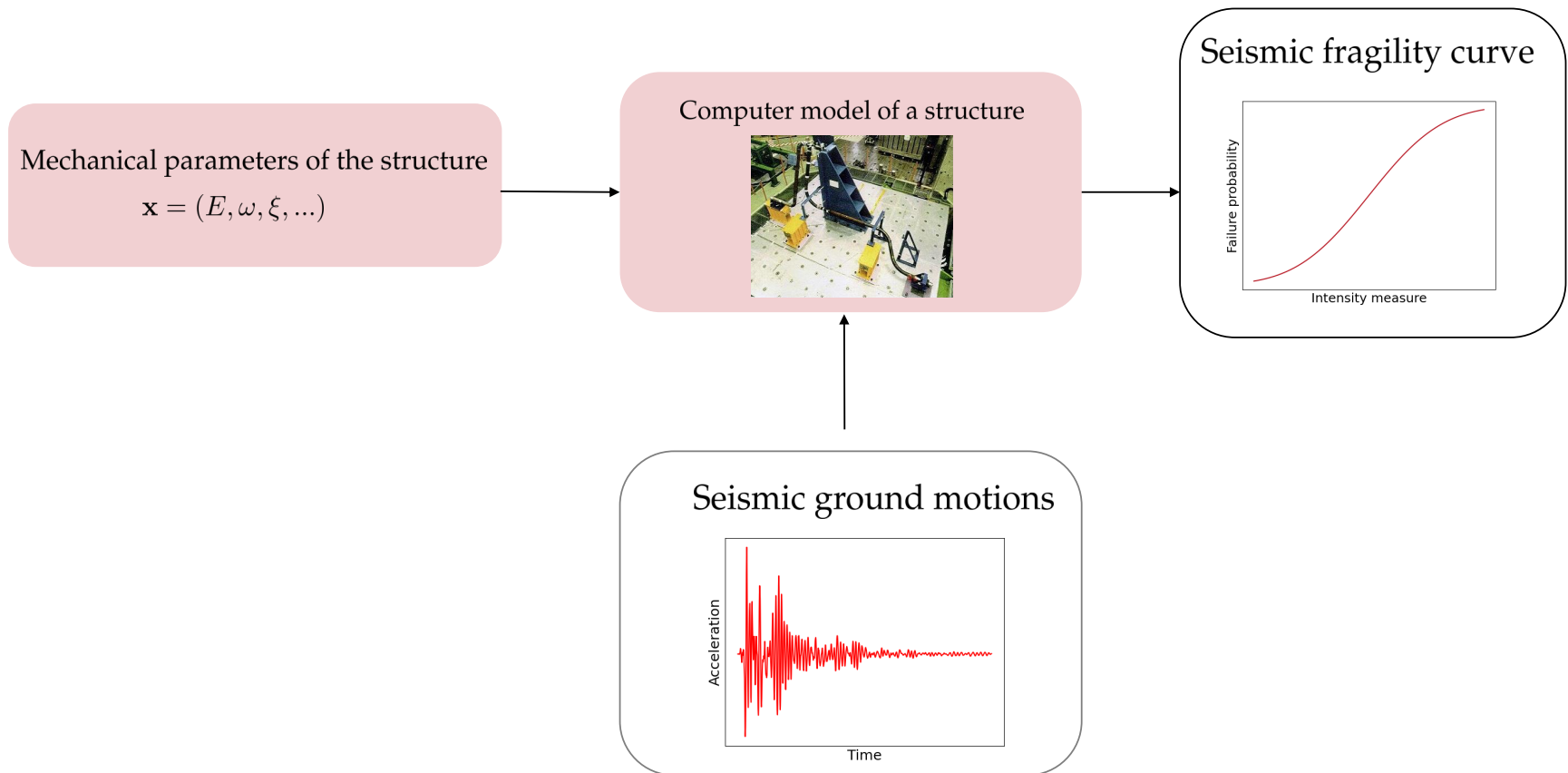
\hookrightarrow This thesis focuses on the second step.

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$$\psi(a) = \mathbb{P}(Z > C | A = a)$$

- **Z**: Mechanical demand of the structure, obtained using time-consuming numerical simulations;
- **C**: Critical level for which the structure is considered in a failure state;
- **A**: Intensity measure of a seismic ground motion. Scalar value representing the intensity of the temporal seismic signal.





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The seismic capacity A_c is defined by

$$A_c = A_m \varepsilon_R \varepsilon_U ,$$

where A_m is the median capacity, ε_R and ε_U follow lognormal distributions with unit median.

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Fragility curve evaluation

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Goal: Data-driven assessment of epistemic uncertainties on seismic fragility curves using computer simulations → Uncertainty Quantification (UQ) methodology.

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- ① Uncertainty Quantification
- ② Surrogate modeling of computer codes using Gaussian process
- ③ Global sensitivity analysis on seismic fragility curves
- ④ Sequential design of experiments
- ⑤ Conclusion and perspectives

- ① **Uncertainty Quantification**
 - General framework
 - Extension to earthquake engineering
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UQ is an interdisciplinary framework aiming to assess the uncertainties tainting a complex engineering system⁴. It has several objectives:

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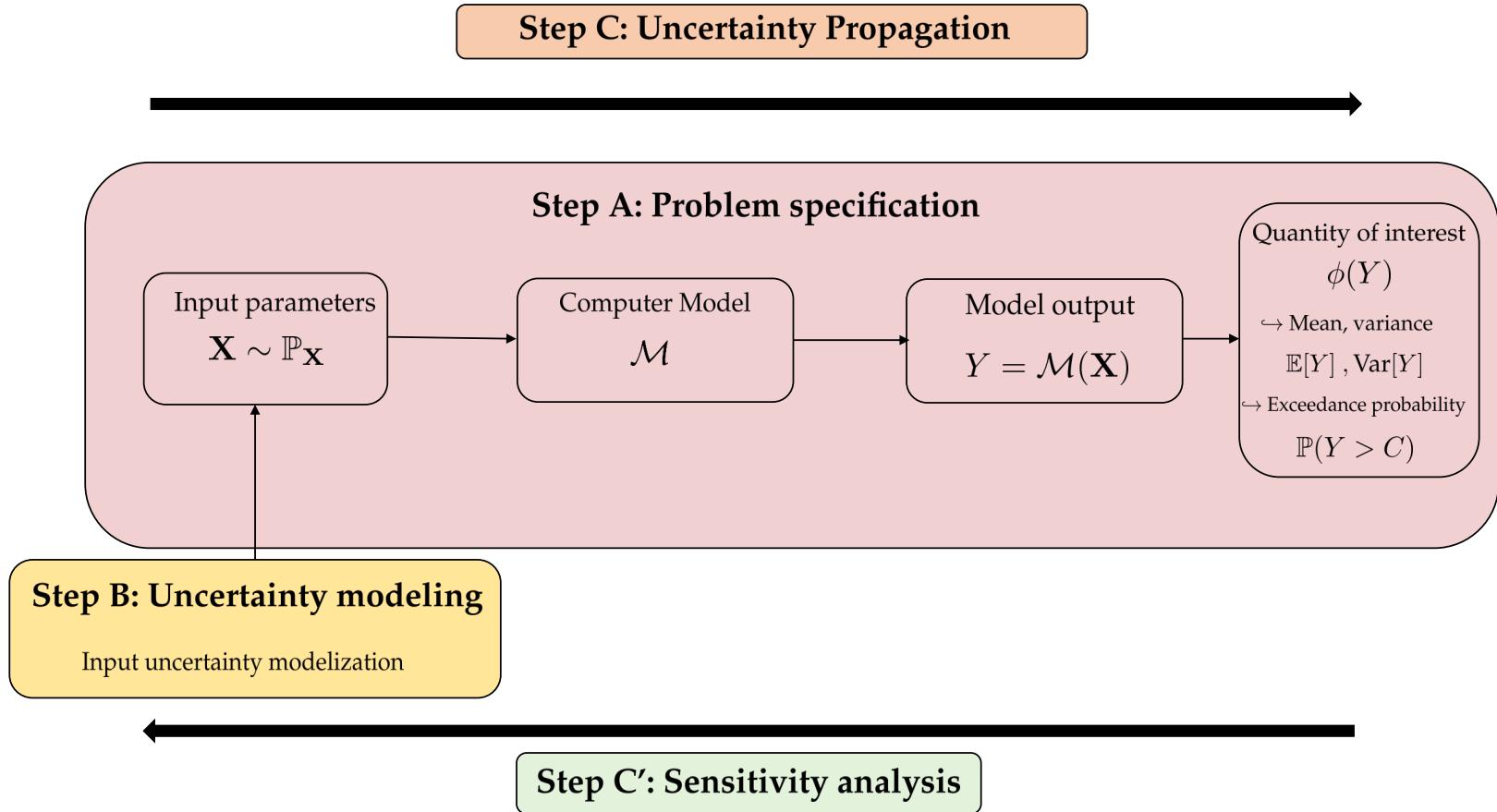
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The computer model of the engineering system is modeled as a function $\mathcal{M} : \mathbb{R}^p \mapsto \mathbb{R}$

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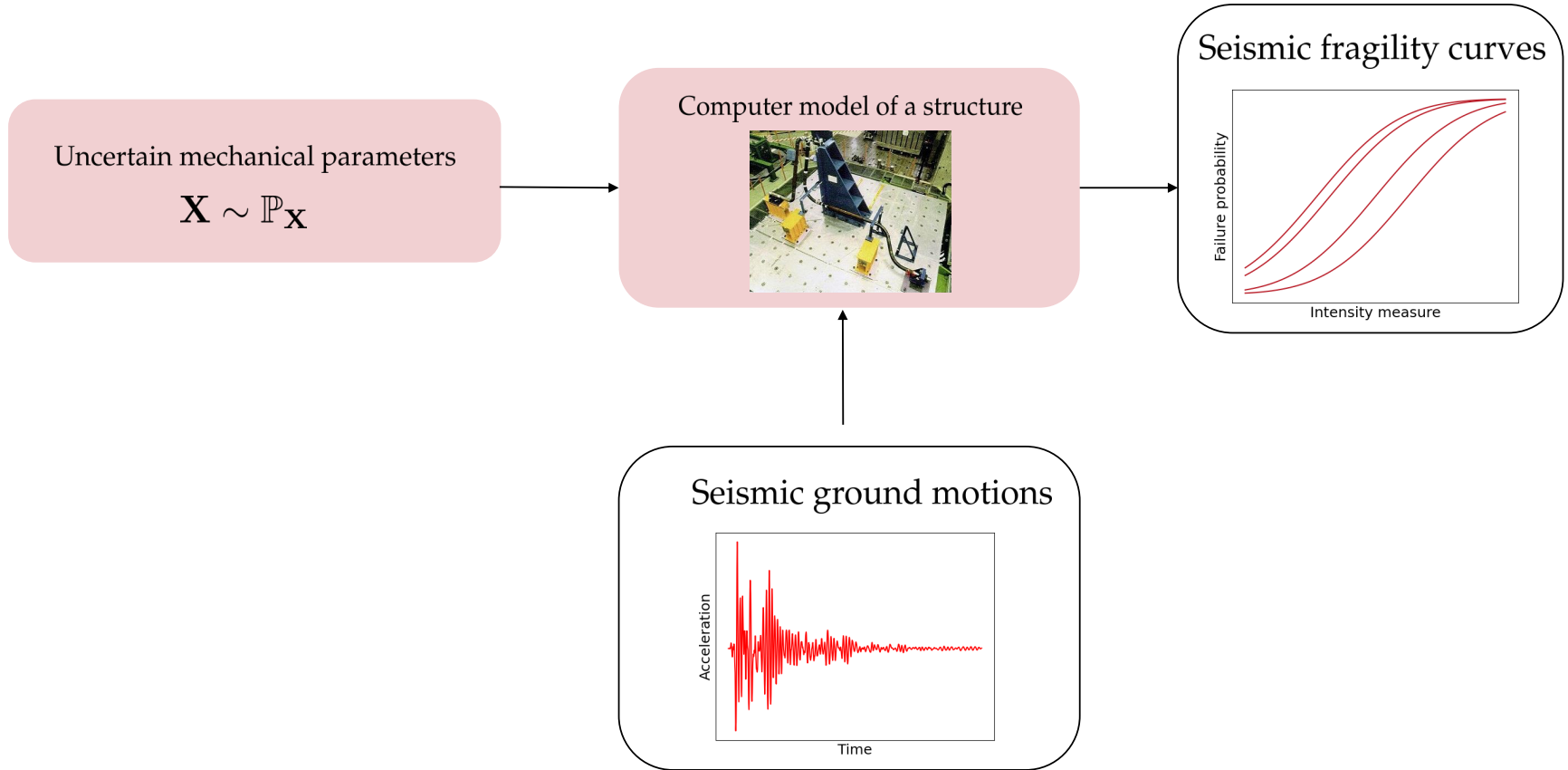


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- ↪ **Our contribution: Adaptation of the UQ framework to earthquake engineering.**



We propose a new definition of fragility curves encompassing mechanical parameters uncertainties.

$$\Psi(a, \mathbf{X}) = \mathbb{P}(z(\mathbf{A}, \mathbf{X}) > C | \mathbf{A} = a, \mathbf{X})$$

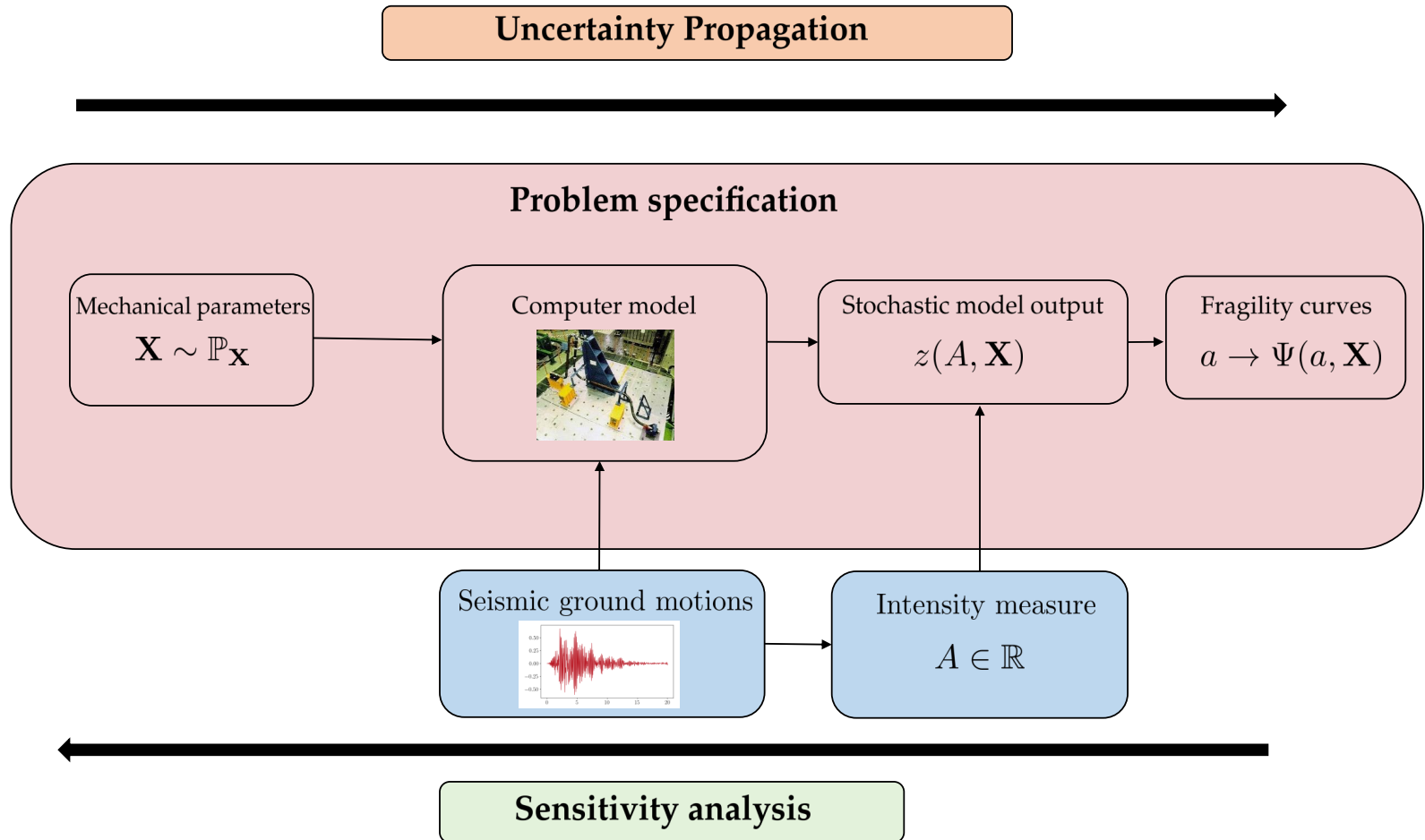
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z is the **stochastic** model output. Its randomness comes from the seismic ground motion uncertainty.



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- **Our contribution:** The seismic fragility quantile curves of level $\gamma \in [0, 1]$

$$q_{\gamma}(a) = \inf_{q \in \mathbb{R}} \left\{ \mathbb{P}_{\mathbf{X}}(\Psi(a, \mathbf{X}) \leq q) \geq \gamma \right\} .$$

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These quantities are untractable to estimate directly using a mechanical computer code \Rightarrow Use of surrogate model.

- ① Uncertainty Quantification
- ② Surrogate modeling of computer codes using Gaussian processes
 - Seismic fragility curves estimation with Gaussian processes.
 - Uncertainty propagation
 - Application to a piping system of a French PWR
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A statistical model has to be proposed on the mechanical computer model output $z(\mathbf{a}, \mathbf{x})$:

$$\mathbf{y}(\mathbf{a}, \mathbf{x}) = \mathbf{g}(\mathbf{a}, \mathbf{x}) + \boldsymbol{\varepsilon}(\mathbf{a}, \mathbf{x}) ,$$

where $\boldsymbol{\varepsilon} \sim \mathcal{N}(\mathbf{0}, \boldsymbol{\sigma}_{\boldsymbol{\varepsilon}}^2(\mathbf{a}, \mathbf{x}))$ and $\mathbf{y}(\mathbf{a}, \mathbf{x}) = \log(z(\mathbf{a}, \mathbf{x}))$.

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The seismic fragility model in this model boils down to

$$\Psi(\mathbf{a}, \mathbf{x}; \mathbf{g}) = \Phi \left(\frac{\mathbf{g}(\mathbf{a}, \mathbf{x}) - \log(C)}{\sigma_\varepsilon(\mathbf{a}, \mathbf{x})} \right) ,$$

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↪ Objective: Build a surrogate model to learn the regression function \mathbf{g} .

Main principle → Predict $y(\mathbf{a}, \mathbf{x})$ using a learning dataset $(\mathbf{a}_i, \mathbf{x}_i, y(\mathbf{a}_i, \mathbf{x}_i))_{1 \leq i \leq n}$.

⁶C. Soize and R. Ghanem. Physical systems with random uncertainties: Chaos representations with arbitrary probability measure.

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Gaussian process (GP) regression has the main advantage to propose an uncertainty on its prediction.

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The uncertainty on the regression function g is modeled by a Gaussian process G with a mean function m and a covariance function Σ_θ . The statistical model becomes

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Given a learning set $\mathcal{D}_n = (\mathbf{a}_i, \mathbf{x}_i, \mathbf{y}(\mathbf{a}_i, \mathbf{x}_i))_{1 \leq i \leq n}$, we can obtain the posterior distribution

$$(G(\mathbf{a}, \mathbf{x}) | \mathcal{D}_n) \sim \mathcal{N}(\hat{G}_n(\mathbf{a}, \mathbf{x}), \hat{\sigma}_n(\mathbf{a}, \mathbf{x})^2) ,$$

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↪ A posterior distribution is obtained on the regression function g .

Given a learning dataset \mathcal{D}_n , we can estimate the seismic fragility curve using the posterior mean.

$$\Psi^{(1)}(a, \mathbf{x}) = \mathbb{E}_{\mathbf{G}} [\Psi(a, \mathbf{x}; \mathbf{G}) | \mathcal{D}_n] ,$$

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where $\sigma_n(\mathbf{a}, \mathbf{x})^2 = \hat{\sigma}_n(\mathbf{a}, \mathbf{x})^2 + \sigma_\varepsilon(\mathbf{a}, \mathbf{x})^2$.

$\Psi^{(1)}$ is **deterministic**.

The advantage of the GP surrogate model is the possibility to propagate its uncertainty on the seismic fragility curve

$$\Psi^{(2)}(a, \mathbf{x}) = \Phi \left(\frac{G_n(a, \mathbf{x}) - \log(C)}{\sigma_\varepsilon(a, \mathbf{x})} \right),$$

where $G_n \stackrel{\mathcal{L}}{=} (G|\mathcal{D}_n)$.

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$\Psi^{(2)}$ is **random** (due to G_n).

- **Plug-in estimator.** Consider a Monte-Carlo sample $(\mathbf{X}_j)_{1 \leq j \leq m}$.

$$q_\gamma^{(1)}(a) = \inf_{q \in \mathbb{R}} \left\{ \frac{1}{m} \sum_{j=1}^m \mathbb{1}_{(\Psi^{(1)}(a, \mathbf{X}_j) \leq q)} \geq \gamma \right\}.$$

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- **Bi-level seismic fragility quantile.** Consider a sample $(\Psi_p^{(2)})_{1 \leq p \leq P}$ of $\Psi^{(2)}$.

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$$q_{\gamma_G, \gamma}^{(2)}(a) = \inf_{q \in \mathbb{R}} \left\{ \frac{1}{m} \sum_{j=1}^m \mathbb{1}_{(q_{\gamma_G}^{(2)}(a, \mathbf{X}_j) \leq q)} \geq \gamma \right\}$$

$\hookrightarrow q_{\gamma_G, \gamma}^{(2)}$ is a bi-level seismic fragility quantile curve (GP uncertainty + epistemic uncertainties).

Industrial use case: The *Alimentation de Secours Générale* (ASG) piping system, equipping French nuclear power plants.

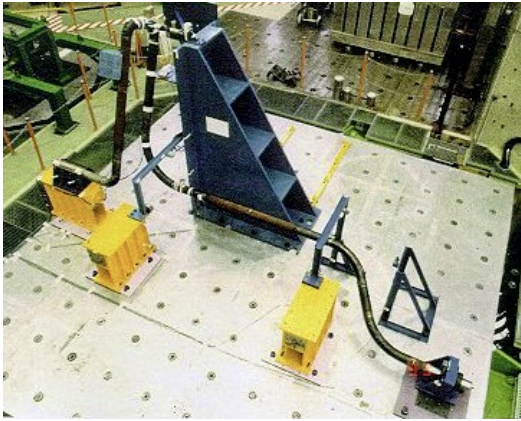


Figure: A view of the ASG piping model on the Azalée shaking table at CEA Saclay

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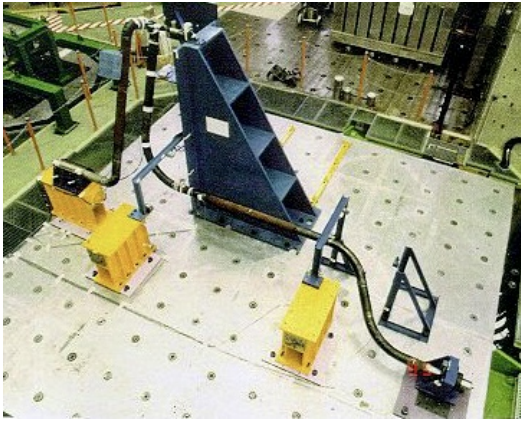


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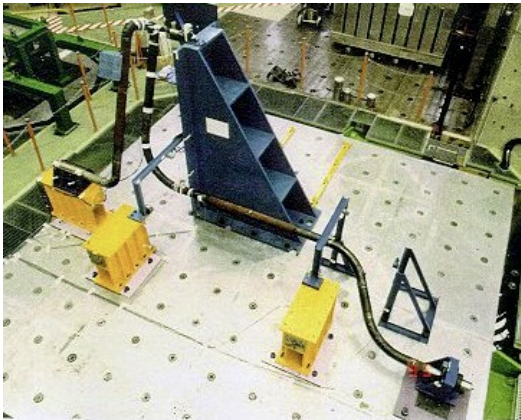


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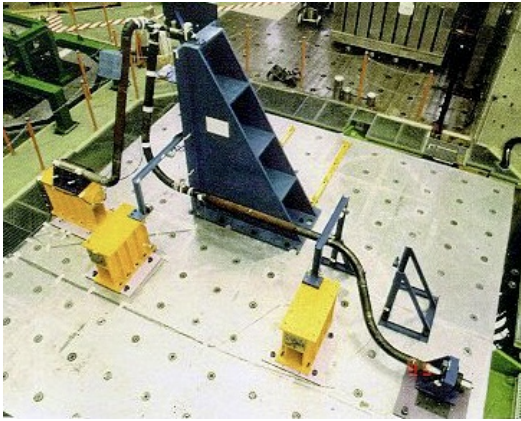


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Industrial use case: The *Alimentation de Secours Générale* (ASG) piping system, equipping French nuclear power plants.

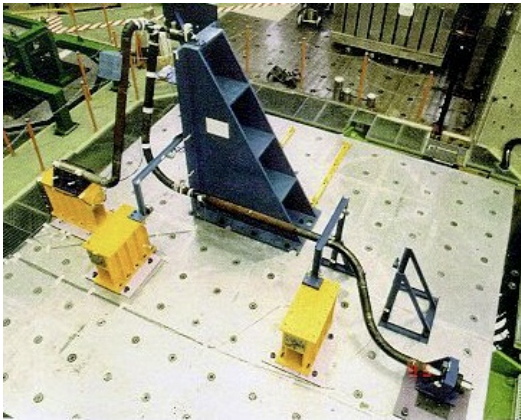


Figure: A view of the ASG piping model on the Azalée shaking table at CEA Saclay

- CAST3M finite element code simulating the dynamic behavior of the piping system validated on the basis of experimental tests ⁷;
- Ten structural parameters (Boundary conditions, mechanical characteristics);
- A quantity of interest for the reliability of the structure: the out-of-plane rotation of a pipe elbow;
- Computational cost of 1 CAST3M call \approx 1 minute \Rightarrow 100 days of computation time for uncertainty propagation.

⁷F. Touboul, P. Sollogoub, and N. Blay. *Seismic behaviour of piping systems with and without defects: experimental and numerical evaluations.*

Nuclear Engineering and Design, 192(2):243–260, 1999

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- ↪ **Boundary conditions:** Translation and rotation stiffness at the clamped end and in the guide.

<i>Variable number</i>	<i>Variable</i>
1	E: Young modulus
2	Sy: Elasticity limit
3	H: Hardening module
4	b: Modal damping ratio
5	RPY151: Rotation stiffness for the P151 guide in Y direction
6	RPX29: Rotation stiffness for the P29 clamped end in X direction
7	RPY29: Rotation stiffness for the P29 clamped end in Y direction
8	TPX29: Translation stiffness for the P29 clamped end in X direction
9	TPY29: Translation stiffness for the P29 clamped end in Y direction
10	TPZ29: Translation stiffness for the P29 clamped end in Z direction

↪ Material parameters

↪ Boundary conditions parameters

- The seismic intensity measure chosen is the spectral acceleration at pulsation $f = 5$ Hz and damping ratio $\xi = 0.01$

$$a = \max_{t \in [0, T]} (2\pi f)^2 |\ell(t)| ,$$

where ℓ is the displacement of a single d.o.f. oscillator;

⁸A. Marrel, B. Iooss, and V. Chabridon. The icscream methodology: Identification of penalizing configurations in computer experiments using screening and metamodel—applications in thermal-hydraulics.

Nuclear Science and Engineering, 196(3):301–321, 2022

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Two Gaussian processes are proposed as surrogates for the mechanical computer code.

They are both **zero mean** with a **tensorized anisotropic Matérn 5/2** covariance function.

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Heteroskedastic model motivation → Mechanical nonlinearities for high intensity seismic ground motions.

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Table: Q^2 numerical values estimated by leave-one-out.

↪ Same predictive performance for the two models.

Credible intervals of level $\alpha \in [0, 1]$

$$\text{CI}_\alpha(\mathbf{a}, \mathbf{x}) = \left[\hat{G}_n(\mathbf{a}, \mathbf{x}) - q_{1-\frac{\alpha}{2}} \sigma_n(\mathbf{a}, \mathbf{x}), \hat{G}_n(\mathbf{a}, \mathbf{x}) + q_{1-\frac{\alpha}{2}} \sigma_n(\mathbf{a}, \mathbf{x}) \right],$$

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Coverage probability of level α

$$\text{CP}_\alpha = \mathbb{P}(\mathbf{y}(\mathbf{A}, \mathbf{X}) \in \text{CI}_\alpha(\mathbf{A}, \mathbf{X})).$$

\hookrightarrow Similarity measure between the data distribution and the GP posterior distribution.

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Empirical estimator on a test dataset $(\mathbf{a}'_i, \mathbf{x}'_i, \mathbf{y}(\mathbf{a}'_i, \mathbf{x}'_i))_{1 \leq i \leq n'}$ or by cross-validation.

$$\widehat{\text{CP}}_\alpha = \frac{1}{n'} \sum_{i=1}^{n'} \mathbb{1}_{\mathbf{y}(\mathbf{a}'_i, \mathbf{x}'_i) \in \text{CI}_\alpha(\mathbf{a}'_i, \mathbf{x}'_i)}.$$

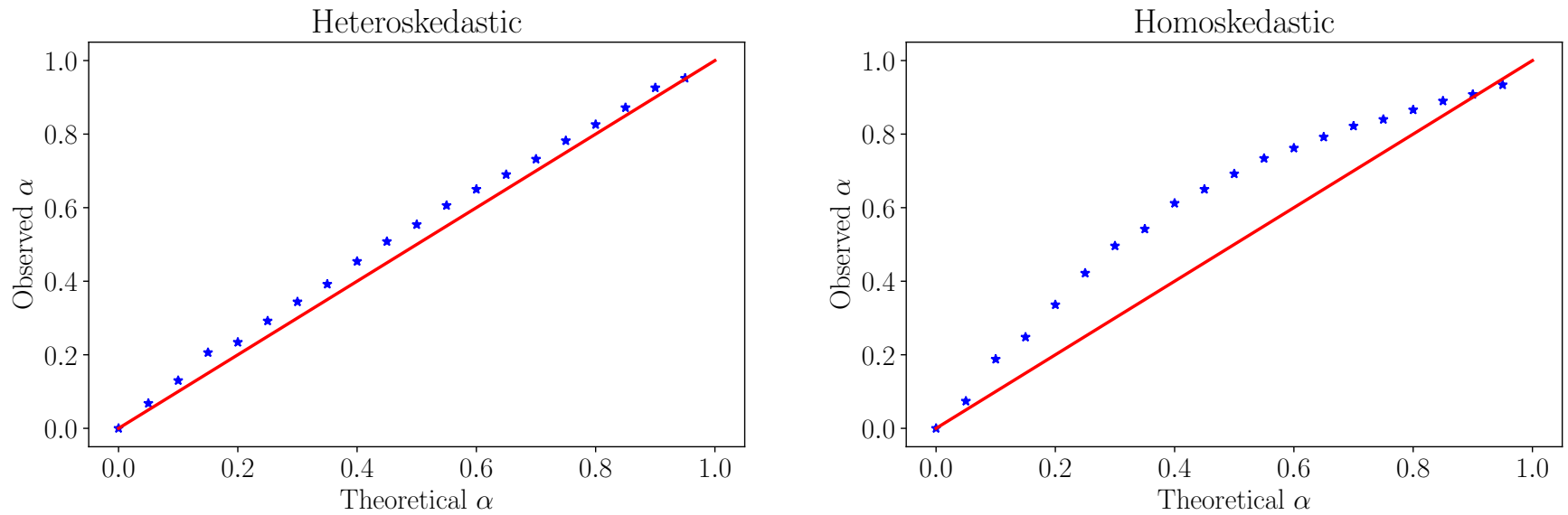


Figure: Leave-one-out estimation of the coverage probabilities.

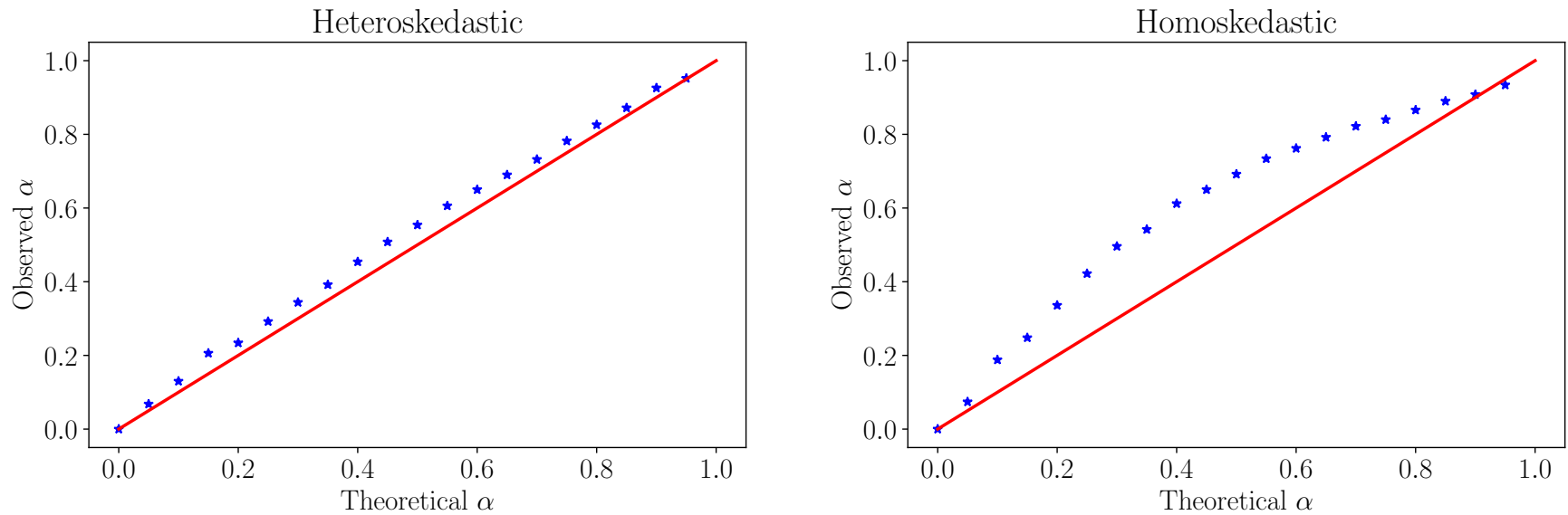
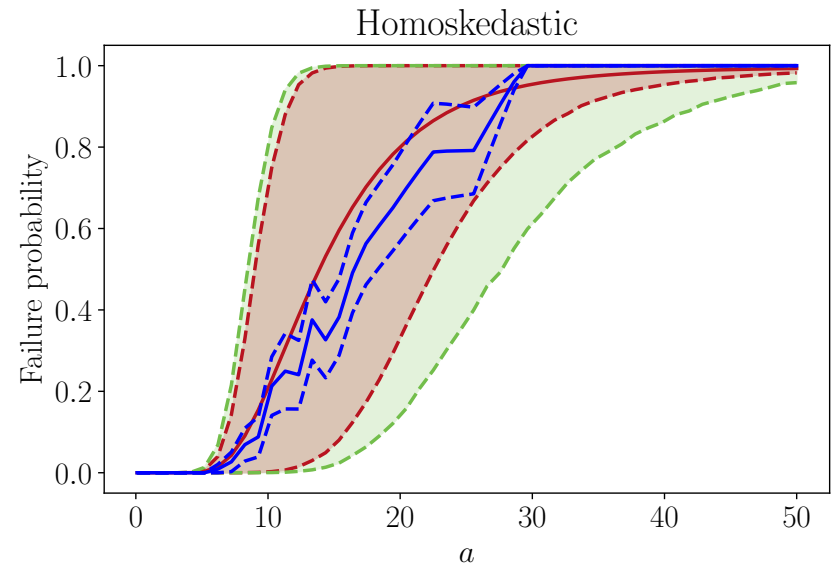
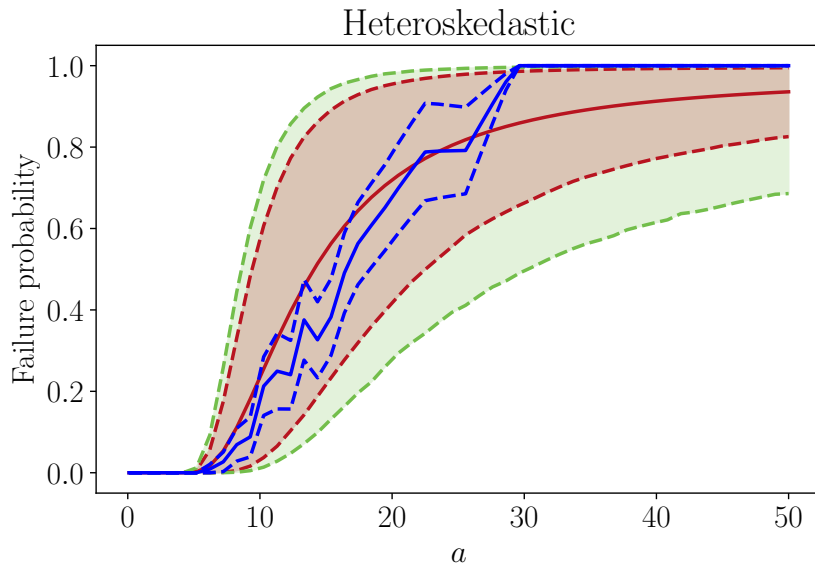


Figure: Leave-one-out estimation of the coverage probabilities.

↪ Better coverage probabilities with the heteroskedastic model.



- $n = 500$ CAST3M computations
- Plug-in quantile curve estimator ($\gamma = 0.1$ and $\gamma = 0.9$)
- Bi-level quantile curves estimator ($\gamma = \gamma_G = 0.1$ and $\gamma = \gamma_G = 0.9$)
- Nonparametric estimation of the mean curve (2000 CAST3M computations)

- 1 Uncertainty Quantification
- 2 Surrogate modeling of computer codes using Gaussian processes
- 3 Global sensitivity analysis on seismic fragility curves**
 - Aggregated Sobol' indices
 - Kernel methods
 - Application
- 4 Sequential design of experiments
- 5 Conclusion and perspectives

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Model inputs → Mechanical parameters of the structure

Model output → Seismic fragility curve

The aggregated Sobol' indices are a natural extension of Sobol' indices to a functional output ¹¹.

¹¹B. Iooss and L. Le Gratiet. *Uncertainty and sensitivity analysis of functional risk curves based on Gaussian processes*. *Reliability Engineering & System Safety*, 187:58–66, 2019

The aggregated Sobol' indices are a natural extension of Sobol' indices to a functional output ¹¹.

Using the notation $\mathbf{X} = (\mathbf{X}^{(1)}, \dots, \mathbf{X}^{(p)})$

$$D = \int_{\mathcal{A}} \text{Var}(\Psi(\mathbf{a}, \mathbf{X})) d\mathbf{h}(\mathbf{a})$$

$$S_i^{\text{FC}} = \frac{1}{D} \int_{\mathcal{A}} \text{Var} \left(\mathbb{E}[\Psi(\mathbf{a}, \mathbf{X}) | \mathbf{X}^{(i)}] \right) d\mathbf{h}(\mathbf{a})$$

is the first-order aggregated Sobol' index of $\mathbf{X}^{(i)}$.

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The probability measure $\mathbf{h} \rightarrow$ Choice of the practitioner.

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Our contribution: ANOVA decomposition of the aggregated Sobol' indices.

Proposition

The aggregated Sobol' indices follow a ANOVA decomposition

$$\sum_{u \subseteq \{1, \dots, p\}} S_u^{FC} = 1,$$

where $\mathbf{X}^{(u)} = (\mathbf{X}^{(j)})_{j \in u}$ and
 $S_u^{FC} = \sum_{v \subseteq u} (-1)^{|u|-|v|} \int_{\mathcal{A}} \text{Var} (\mathbb{E}[\Psi(\mathbf{a}, \mathbf{X}) | \mathbf{X}^{(v)}]) d\mathbf{h}(\mathbf{a})$.

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↔ The total-order aggregated Sobol' indices are thus well-defined

$$T_i^{FC} = 1 - \frac{1}{D} \int_{\mathcal{A}} \text{Var} \left(\mathbb{E}[\Psi(\mathbf{a}, \mathbf{X}) | \mathbf{X}^{(-i)}] \right) d\mathbf{h}(\mathbf{a}),$$

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Recently, global sensitivity indices based on kernels have been proposed ¹².

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Theoretical guarantees → ANOVA decomposition ¹³.

Motivation: Kernels methods are adapted to complex data types.

↔ Definition of kernel based global sensitivity indices tailored for seismic fragility curves.

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Consider a Reproducing Kernel Hilbert Space (RKHS) \mathcal{H} with reproducing kernel $k : \mathcal{X} \times \mathcal{X} \mapsto \mathbb{R}$ and dot product $\langle \cdot, \cdot \rangle_{\mathcal{H}}$.

The **kernel mean embedding** $m_{\mu} \in \mathcal{H}$ of a probability measure μ is defined by

$$m_{\mu} = \int_{\mathcal{X}} k(\mathbf{x}, \cdot) d\mu(\mathbf{x}) .$$

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Practical expression of the MMD ¹⁴

$$\text{MMD}^2(\mu, \nu) = \mathbb{E}_{U, U' \sim \mu}[k(U, U')] + \mathbb{E}_{V, V' \sim \nu}[k(V, V')] - 2\mathbb{E}_{U \sim \mu, V \sim \nu}[k(U, V)] .$$

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The β^k indices are generalized global sensitivity indices ¹⁵ defined using Maximum Mean Discrepancy (MMD) distance.

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The first-order β_i^k and total-order β_{-i}^k indices of variable $\mathbf{X}^{(i)}$ are defined by:

$$\beta_i^k = \frac{\mathbb{E}_{\mathbf{X}^{(i)}} \left[\text{MMD}^2 \left(\mathbb{P}_{\Psi}, \mathbb{P}_{\Psi|\mathbf{X}^{(i)}} \right) \right]}{\text{MMD}_{\text{tot}}^2},$$

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$$\text{MMD}_{\text{tot}}^2 = \mathbb{E}[k(\Psi(\cdot, \mathbf{X}), \Psi(\cdot, \mathbf{X}))] - \mathbb{E}_{\mathbf{X}, \mathbf{X}'}[k(\Psi(\cdot, \mathbf{X}), \Psi(\cdot, \mathbf{X}'))].$$

↔ ANOVA decomposition for the β^k -indices¹⁶.

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A *pick-freeze* formulation ¹⁷ has been proposed to estimate the aggregated Sobol' and β^k indices → Large Monte-Carlo samples are needed.

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↪ Adaptation of the kriging conditioning sampling method detailed in Le Gratiet [2013]¹⁸ to noisy observations during the PhD.

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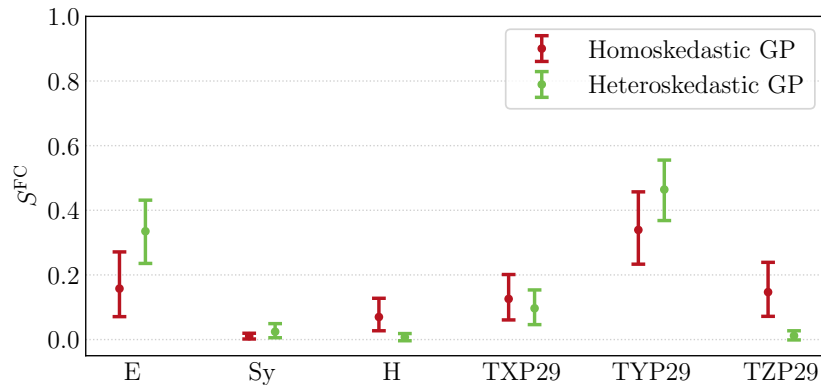
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Global sensitivity analysis for 6 mechanical parameters of the structure

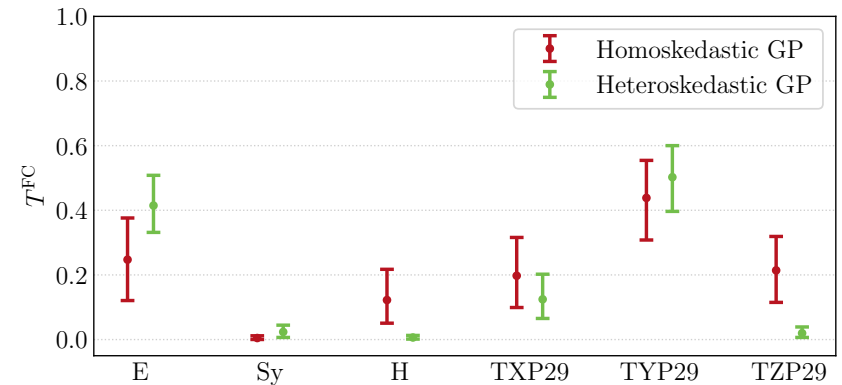
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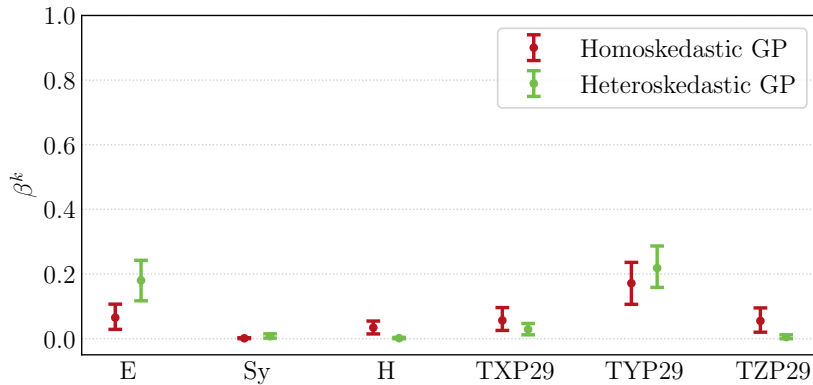


(a) First order

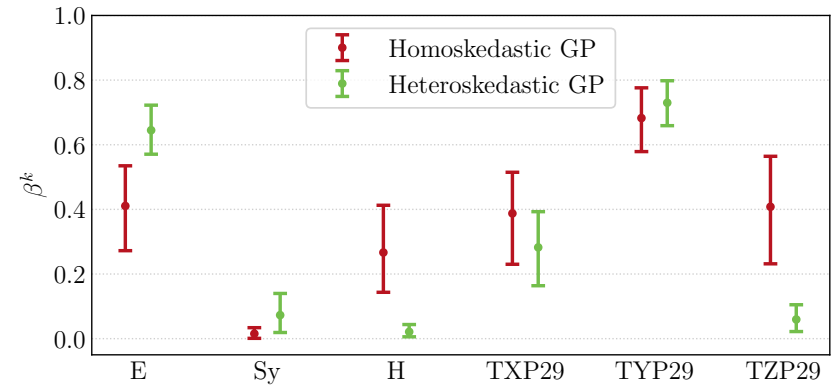


(b) Total order

↪ Graphical representation of the posterior distribution of the aggregated Sobol' indices for the ASG piping system using 300 CAST3M computations.



(a) First order



(b) Total order

$$k(\Psi, \Psi') = \exp\left(-\frac{\|\Psi - \Psi'\|_{L_h^2(\mathcal{A})}^2}{2\ell^2}\right)$$

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- ⑤ Conclusion and perspectives

Goal: Improve the estimation accuracy of seismic fragility curves with a fixed budget of evaluations of the computer code $z(a, \mathbf{x})$.

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²⁰J. Bect, D. Ginsbourger, L. Li, V. Picheny, and E. Vazquez. Sequential design of computer experiments for the estimation of a probability of failure.

Statistics and Computing, 22(3):773–793, 2012

Given $(Y|\mathcal{D}_n) \sim \mathcal{N}(\widehat{G}_n(\mathbf{a}, \mathbf{x}), \widehat{\sigma}_n(\mathbf{a}, \mathbf{x})^2)$ and define

$$\widehat{\Psi}_n(\mathbf{a}, \mathbf{x}) = \Phi \left(\frac{\widehat{G}_n(\mathbf{a}, \mathbf{x}) - \log(C)}{\widehat{\sigma}_n(\mathbf{a}, \mathbf{x})} \right) .$$

The sequential procedure is defined by

$$\mathbf{A}_{n+1}^{\text{SUR}}, \mathbf{X}_{n+1}^{\text{SUR}} = \underset{\mathbf{a}, \mathbf{x} \in \mathcal{A} \times \mathcal{X}}{\text{argmin}} J_n(\mathbf{a}, \mathbf{x}) ,$$

where J_n is the SUR sampling criterion at step n defined by

$$J_n(\mathbf{a}, \mathbf{x}) = \mathbb{E}_{\mathbf{G}} \left[\int_{\mathcal{A} \times \mathcal{X}} (\Psi(\alpha, u; \mathbf{G}) - \widehat{\Psi}_{n+1}(\alpha, u))^2 d\mathbf{h}(\alpha) d\mathbb{P}_{\mathbf{X}}(u) \Big| \mathbf{A}_{n+1} = \mathbf{a}, \mathbf{X}_{n+1} = \mathbf{x}, \mathcal{F}_n \right]$$

\mathcal{F}_n is the σ -algebra generated by \mathcal{D}_n .

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↪ Expression of J_n + Practical methods for its computation.

- 10 randomly chosen realizations are used for initialization;

- 10 randomly chosen realizations are used for initialization;
- At step n , $m = 1000$ candidate points $(A_i, X_i)_{1 \leq i \leq m}$ are subsampled in the dataset of 2000 CAST3M computations. We define:

$$(A_{n+1}^{\text{SUR}}, X_{n+1}^{\text{SUR}}) = \underset{1 \leq i \leq m}{\operatorname{argmin}} J_n(A_i, X_i) .$$

A numerical benchmark is carried out to compare the performance of SUR strategy and Monte-Carlo designs in terms of posterior variance:

$$v_n = \mathbb{E}_G \left[\int_{\mathcal{A} \times \mathcal{X}} (\Psi(\alpha, u; G) - \hat{\Psi}_n(\alpha, u))^2 dh(\alpha) d\mathbb{P}_X(u) \middle| \mathcal{F}_n \right],$$

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and in terms of bias using a reference fragility curve Ψ_{ref} :

$$b_n = \int_{\mathcal{A} \times \mathcal{X}} (\Psi_{\text{ref}}(\alpha, u) - \hat{\Psi}_n(\alpha, u))^2 dh(\alpha) d\mathbb{P}_X(u).$$

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The integral is evaluated with a Monte-Carlo sample of size 5000 and the expectation on G using 4000 realizations of the GP surrogate.

The SUR strategy is compared to a Monte-Carlo design.

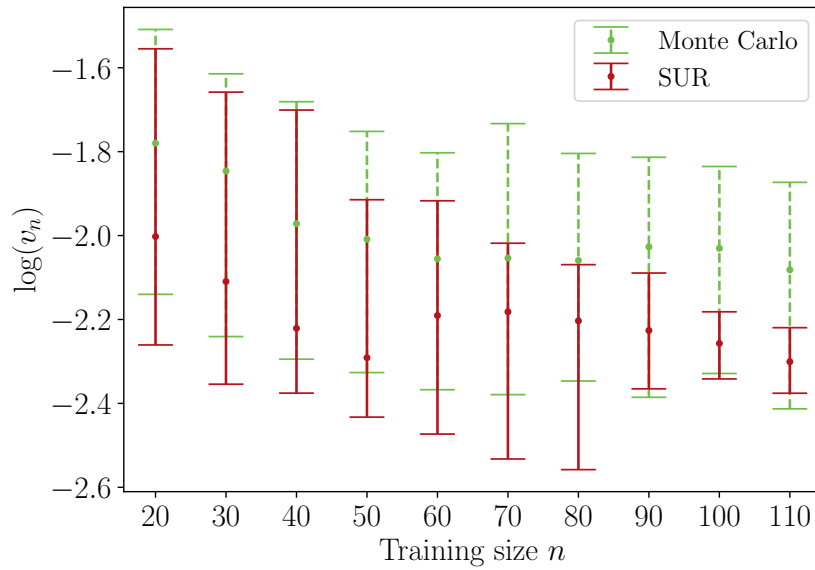
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100 replications of Monte-Carlo designs for several training sizes are computed.

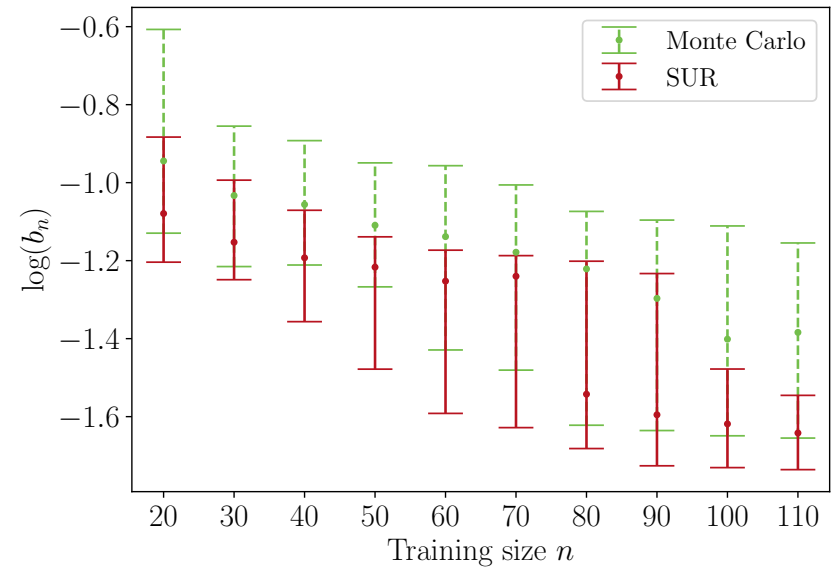
The SUR strategy is compared to a Monte-Carlo design.

100 replications of Monte-Carlo designs for several training sizes are computed.

Due to the randomness induced in the SUR algorithm by choosing the candidate points at each step, 100 runs of the SUR strategy are carried out using HPC.



(a) Performance evaluation on the variance



(b) Performance evaluation on the bias

- ① Uncertainty Quantification
- ② Surrogate modeling of computer codes using Gaussian processes
- ③ Global sensitivity analysis on seismic fragility curves
- ④ Sequential design of experiments
- ⑤ Conclusion and perspectives

- Uncertainty Quantification framework development for earthquake engineering;
- Estimators of seismic fragility curve based on GP surrogates;
- Global sensitivity indices defined on seismic fragility curves;
- Sequential design of experiments
 - ↪ Importance sampling based active learning (frequentist viewpoint)
 - ↪ SUR procedure (Bayesian viewpoint)

C. Gauchy, C. Feau, and J. Garnier. Importance sampling based active learning for parametric seismic fragility curve estimation.

2021.

doi: [10.48550/ARXIV.2109.04323](https://doi.org/10.48550/ARXIV.2109.04323)

C. Gauchy, C. Feau, and J. Garnier. Uncertainty quantification and global sensitivity analysis of seismic fragility curves using kriging.

2022a.

doi: [10.48550/ARXIV.2210.06266](https://doi.org/10.48550/ARXIV.2210.06266)

C. Gauchy, C. Feau, and J. Garnier. Estimation of seismic fragility curves by sequential design of experiments.

In *52ème journées de Statistique de la Société Française de Statistique (JdS 2022)*, Lyon, France, 2022b

- Latent model for heteroskedastic GP regression ²¹;
- Model selection (AIC, BIC, Bayes factor,...);
- Bayesian methodology for seismic fragility curve estimation. Prior elicitation using reference prior theory ²².

²¹A. Marrel, B. Iooss, S. Da Veiga, and M. Ribatet. *Global sensitivity analysis of stochastic computer models with joint metamodels*.

Statistics and Computing, 22(3):833–847, 2012

²²J. O. Berger, J. M. Bernardo, and D. Sun. *The formal definition of reference priors*.

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Thank you for your attention !

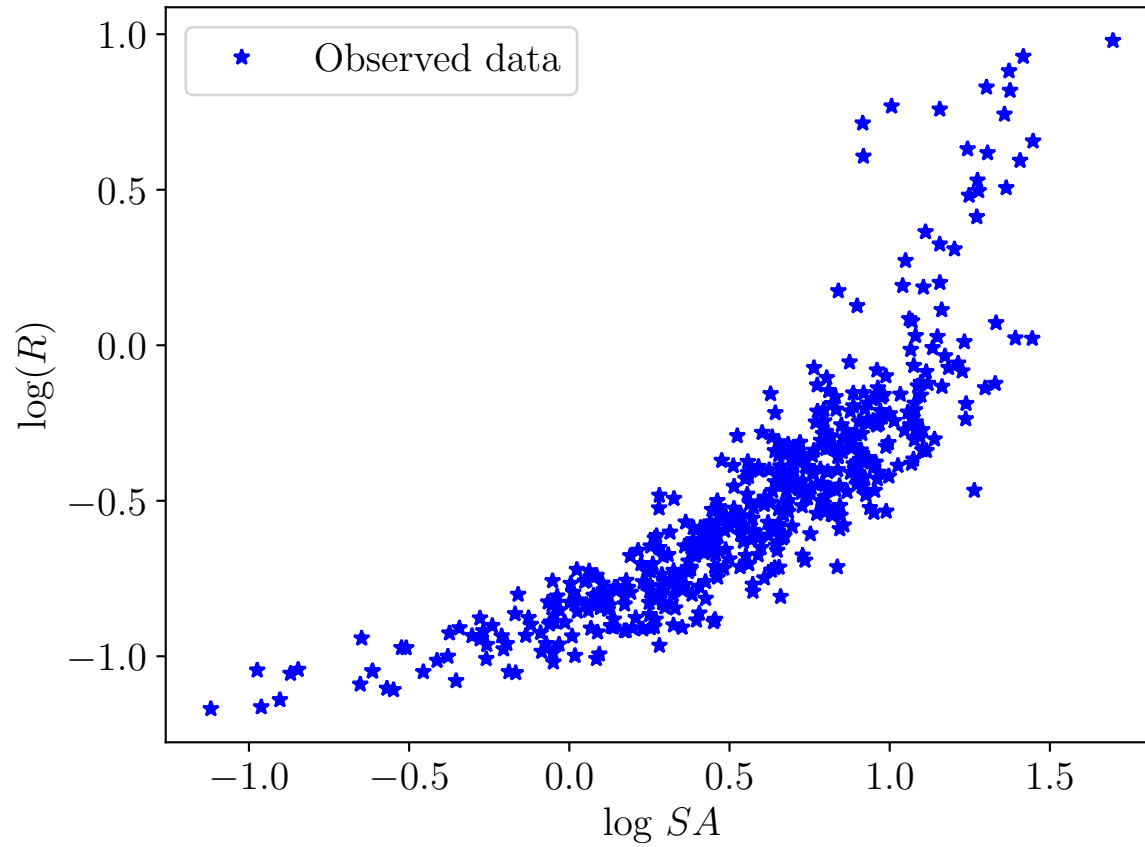
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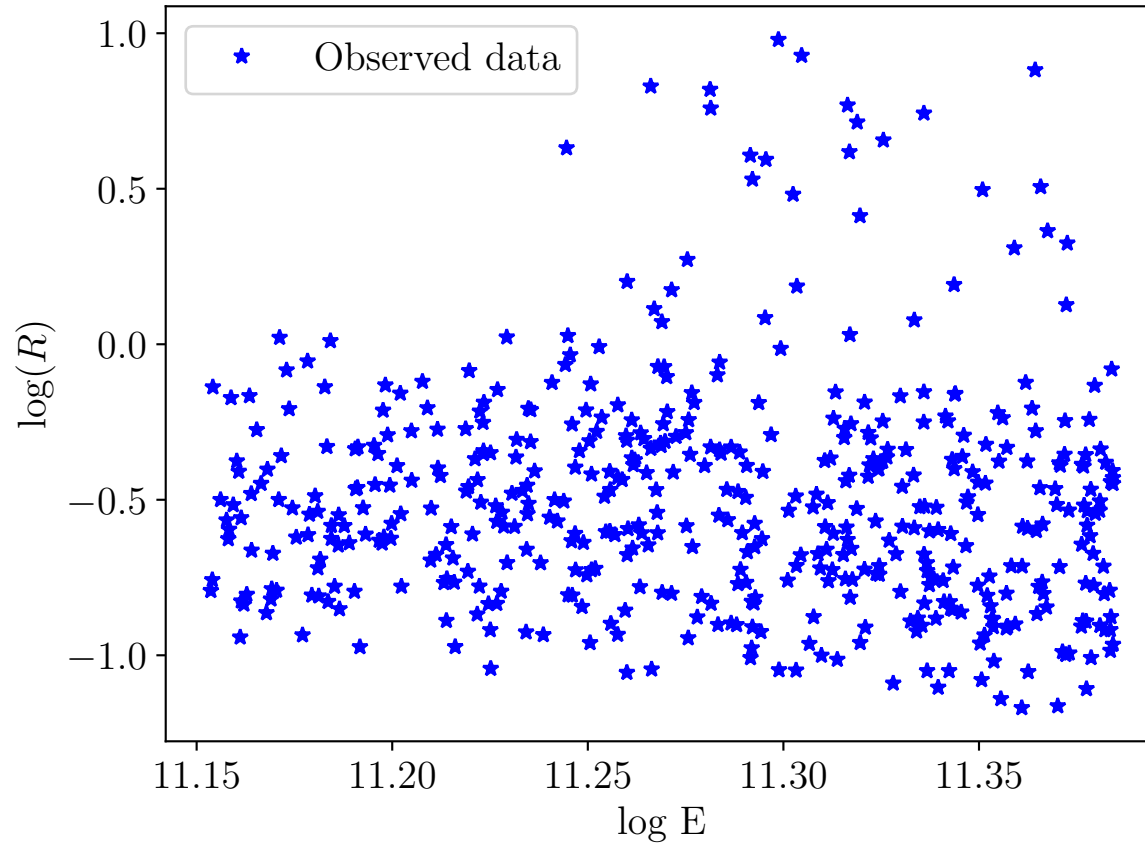
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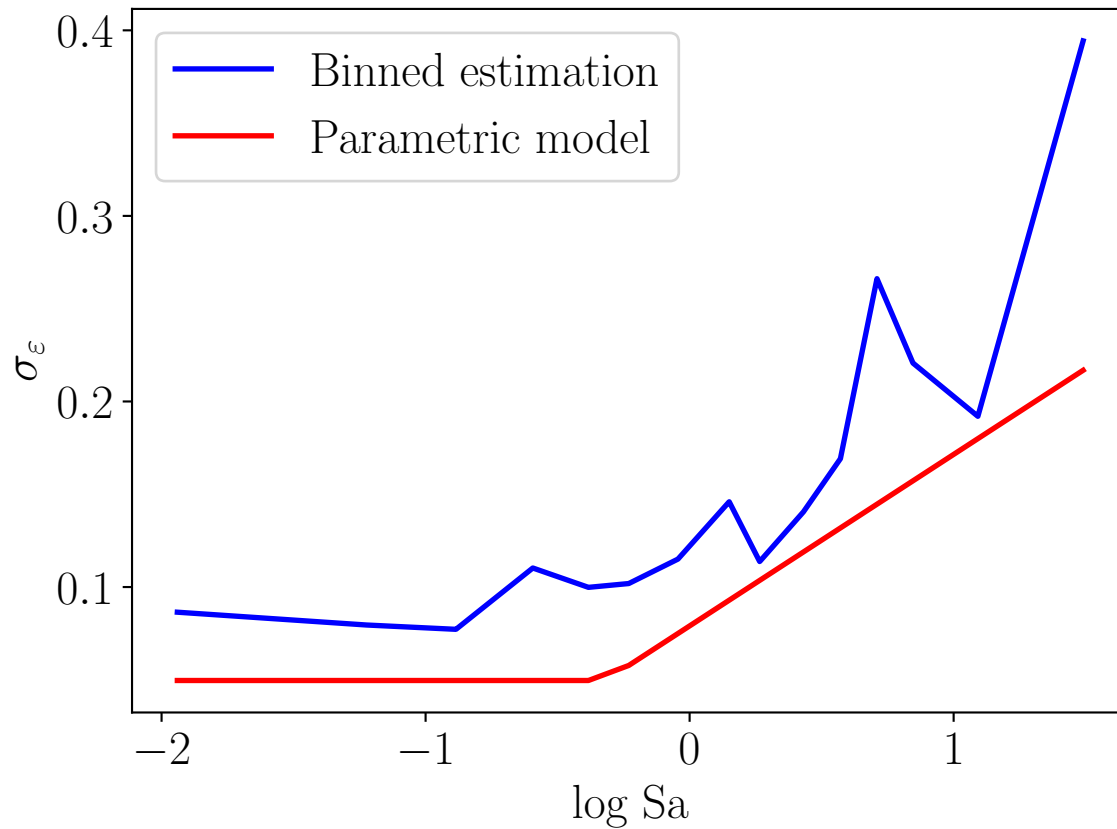
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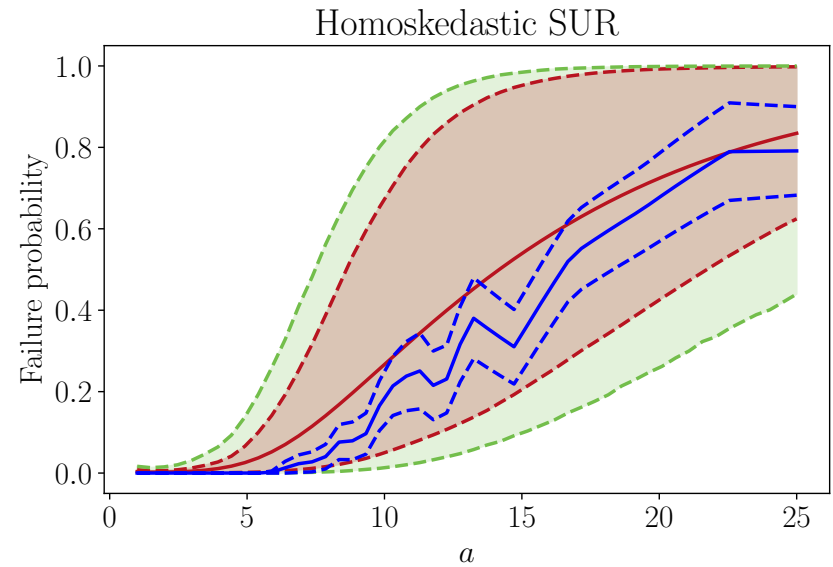
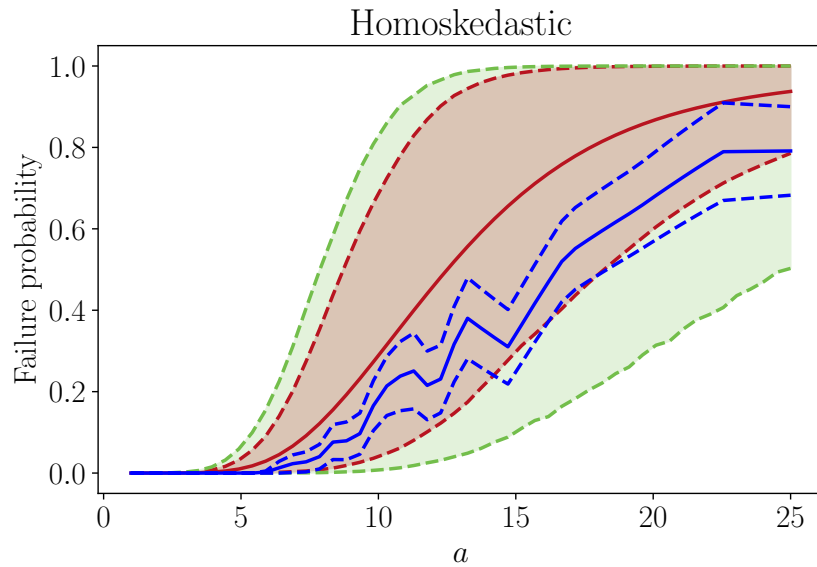
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Given data $(X_i, S_i)_{1 \leq i \leq n}$ where $S_i \in \{0, 1\}$ and $X_i = \log(A_i)$. The fragility curve $\psi(x)$ is just

$$\psi(x) = \mathbb{E}[S|X = x] .$$

Given a function space $\mathcal{F} = \{\psi_\theta, \theta \in \Theta\}$. The goal is to minimize

$$g(\theta) = \mathbb{E}[(\psi(X) - \psi_\theta(X))^2] .$$

In practice optimization is done on the following objective function

$$r(\theta) = \mathbb{E}[(S - \psi_\theta(X))^2] .$$

Empirical estimator:

$$\hat{R}_n(\theta) = \frac{1}{n} \sum_{i=1}^n (S_i - \psi_\theta(X_i))^2 .$$

↪ Importance sampling to reduce the variance of the empirical approximation of $r(\theta)$.

$$\widehat{R}_n^{\text{IS}}(\theta) = \frac{1}{n} \sum_{i=1}^n \frac{p(\mathbf{X}_i)}{q(\mathbf{X}_i)} (S_i - \psi_\theta(\mathbf{X}_i))^2 .$$

The instrumental density q is chosen to minimize the variance:

$$\int_{\mathbf{x}} \frac{p^2(\mathbf{x})}{q(\mathbf{x})} \tilde{\ell}_\theta^2(\mathbf{x}) d\mathbf{x} - r(\theta)^2 ,$$

where $\tilde{\ell}_\theta^2(\mathbf{x}) = \mathbb{E}[(S - \psi_\theta(\mathbf{X}))^4 | \mathbf{X} = \mathbf{x}]$.

Parametric family of lognormal seismic fragility curves: $\mathcal{F} = \left\{ \Phi \left(\frac{\log(IM/\alpha)}{\beta} \right), (\alpha, \beta) \in \Theta \right\}$

Penalization term $\Omega(\theta) = \frac{\beta_{\text{reg}}}{\beta}$

↪ Importance sampling to reduce the variance of the empirical approximation of $r(\theta)$.

$$\widehat{R}_n^{\text{IA}}(\theta) = \frac{1}{n} \sum_{i=1}^n \frac{p(\mathbf{X}_i)}{q_{\widehat{\theta}_{i-1}^{\text{IA}}, \varepsilon}(\mathbf{X}_i)} (S_i - \psi_{\theta}(\mathbf{X}_i))^2 + \frac{\beta_{\text{reg}}}{n\beta},$$

$$\widehat{\theta}_n^{\text{IA}} = \underset{\theta \in \Theta}{\text{argmin}} \widehat{R}_n^{\text{IA}}(\theta)$$

↪ Consistency of $\hat{\theta}_n^{\text{IA}}$. Let $\theta_* = \operatorname{argmin} \mathbb{E}[(\psi(X) - \psi_\theta(X))^2]$,

$$\hat{\theta}_n^{\text{IA}} \xrightarrow[n \rightarrow +\infty]{} \theta_* \text{ in probability.}$$

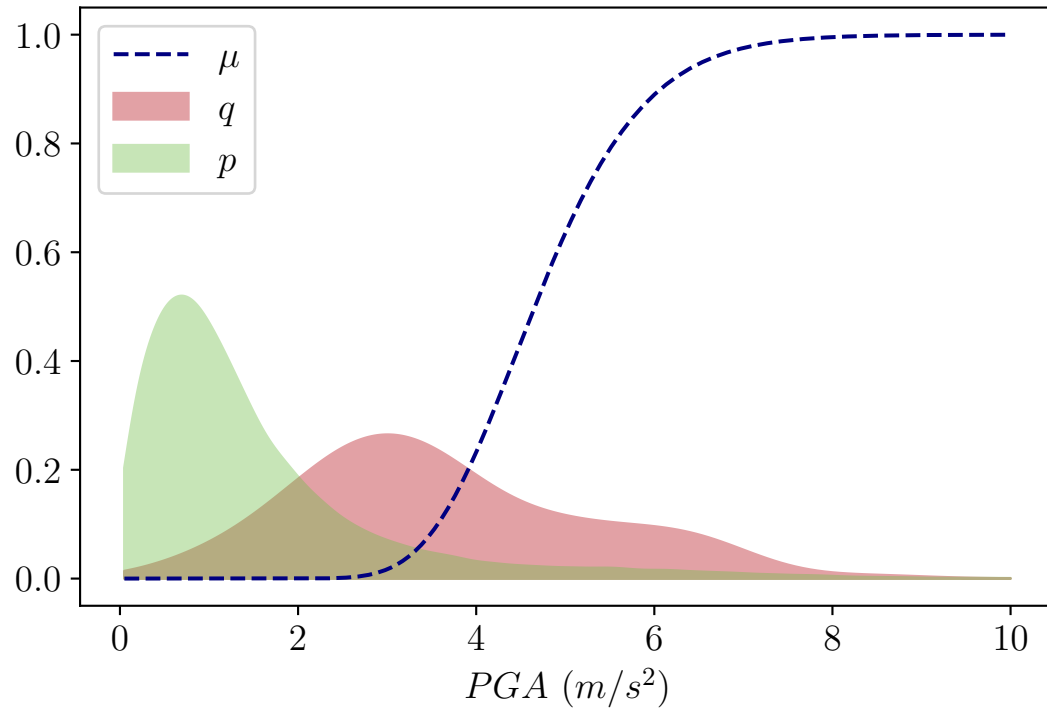
↪ Asymptotic normality of $\hat{\theta}_n^{\text{IA}}$.

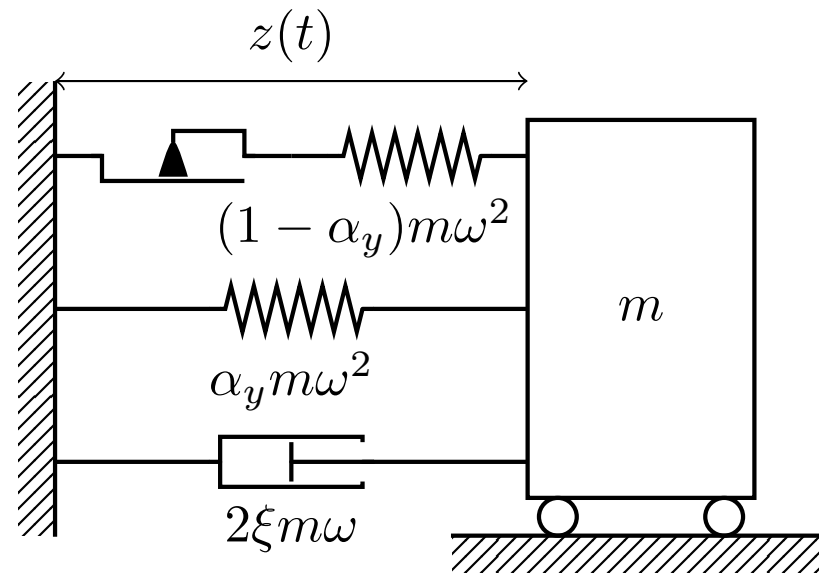
$$\sqrt{n}(\hat{\theta}_n^{\text{IA}} - \theta_*) \xrightarrow{\mathcal{D}} \mathcal{N}(0, G_{\theta_*, \varepsilon}^{-1})$$

Proofs sketch: Combine convergence of martingal results (Hall et al. [2014]²³) with Z-estimation theory (Van der Vaart [1998]²⁴)

²³P. Hall, C.C. Heyde, Z.W. Birnbaum, and E. Lukacs. *Martingale Limit Theory and Its Application*. Communication and Behavior. Elsevier Science, 2014

²⁴A. W. Van der Vaart. *Asymptotic Statistics*. Cambridge Series in Statistical and Probabilistic Mathematics. Cambridge University Press, 1998





$$\ddot{z}(t) + 2\xi\omega\dot{z}(t) + f^{\text{NL}}(z(t)) = -s(t),$$

where f^{NL} is a nonlinear restoring force.

